



Capacity for Rail

# S&C: Understanding Root Causes & Assessing Effective Remedies

C4R Final Dissemination Event, Paris 15<sup>th</sup> March 2017

Presenter:

**Dr Yann Bezin**

Institute of Railway Research, University of Huddersfield



1. Brief review of **key damages** and **root causes** in relation to S&C vehicle-track interaction
2. Understanding/predicting **wheel and rail interaction** at S&C
3. Predicting **damage mechanisms** in rails and support and identifying the **key drivers**
4. Assessing the **benefit of crossing geometry change** and other **innovations** on the system performance

# C4R S&C Failure Catalogue

- #44 Failures catalogued in public Deliverable-13.1
- Presented at 1<sup>st</sup> Dissemination event, Paris June 2015

**1.1 Switch & Stock Rail Assembly**

**1.1.1 SPALLING OF STOCK RAIL**

**Component**

Stock Rail



**Characteristics:** This defect mainly occurs in the wheel transfer area of the switch/stock rail and shows cavities left by material having spalled out.

**(Possible) Causes:**

- High contact stresses leading to near surface crack initiation and subsequent merger to cause spalling. High stress can result from worn wheels (false flange) or non-optimal wheel transfer zone and narrow running bands.
- Wheel flange not matching together with design of wheel transfer zone
- Incorrect profile of wheel flange



**Preventive/corrective measures:**

Deburring, grinding, Replacement of switch and stock rail assembly (improved wheel profile management)

**Detection:**

Visual inspection

013.1 – Operational failure modes of S&C

CAPACITY4RAIL  
SCFD-0A-2013-406430  
2014/06/17

**1. Failure Description**

**1.1 SWITCH AND STOCK RAIL ASSEMBLY**

Title and failure	Language(s)
<b>1.1.1 SPALLING OF STOCK RAIL</b>	Stock rail
<p><b>Characteristics:</b> This defect mainly occurs in the wheel transfer area of the switch/stock rail and shows cavities left by material having spalled out.</p>	
	
<p><b>Causes:</b> High contact stresses leading to near surface crack initiation and subsequent merger to cause spalling. High stress can result from worn wheels (false flange) or non-optimal wheel transfer zone and narrow running bands. Wheel flange not matching together with design of wheel transfer zone Incorrect profile of wheel flange</p>	
<p><b>Appearance:</b> In the wheel transfer area of the switch/stock rail</p>	
<p><b>Corrective/Preventive Measures:</b></p> <p><b>Deburring</b> <b>Grinding</b> Replacement of switch and stock rail assembly (improved wheel profile management) Detected by visual inspection</p>	
<p><b>Remarks:</b></p>	

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# Components damages in S&C



Switch  
and stock  
rails

- Lipping & spalling
- Head checks
- Squats
- wear

Points

- Additional fracture  
by fatigue

Bearers

- Fatigue cracking
- Vertical movement  
and hanging
- Lateral shift

Slide  
plates

- Poor movement  
(high friction)
- Seizure



# Components damages in S&C

- Transverse fatigue crack (foot or nose)

Cast crossing



- Wear
- Plastic deformation
- Shelling & spalling

Crossing nose & Wing



- Excessive Wear

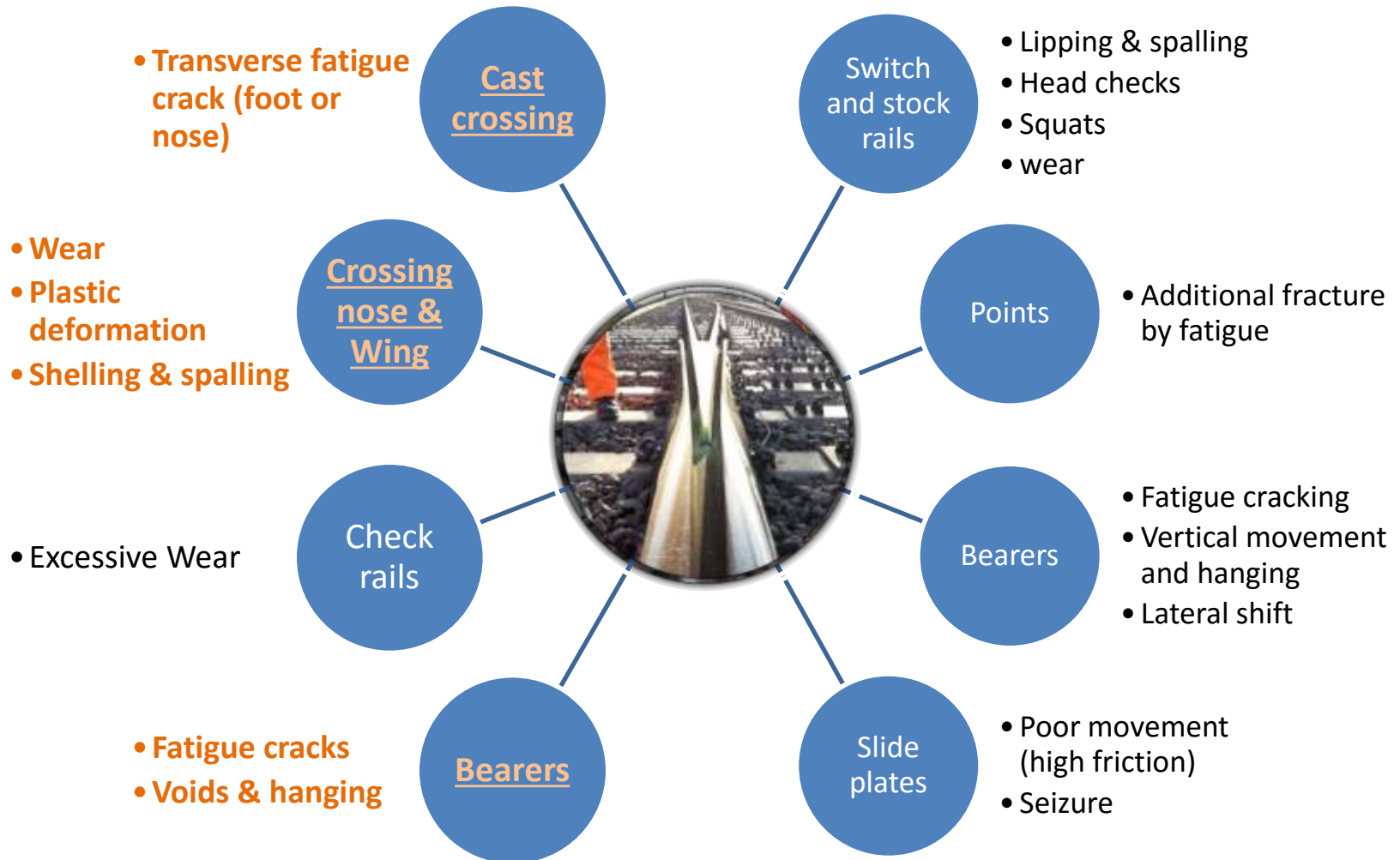
Check rails

- Fatigue cracks
- Voids & hanging

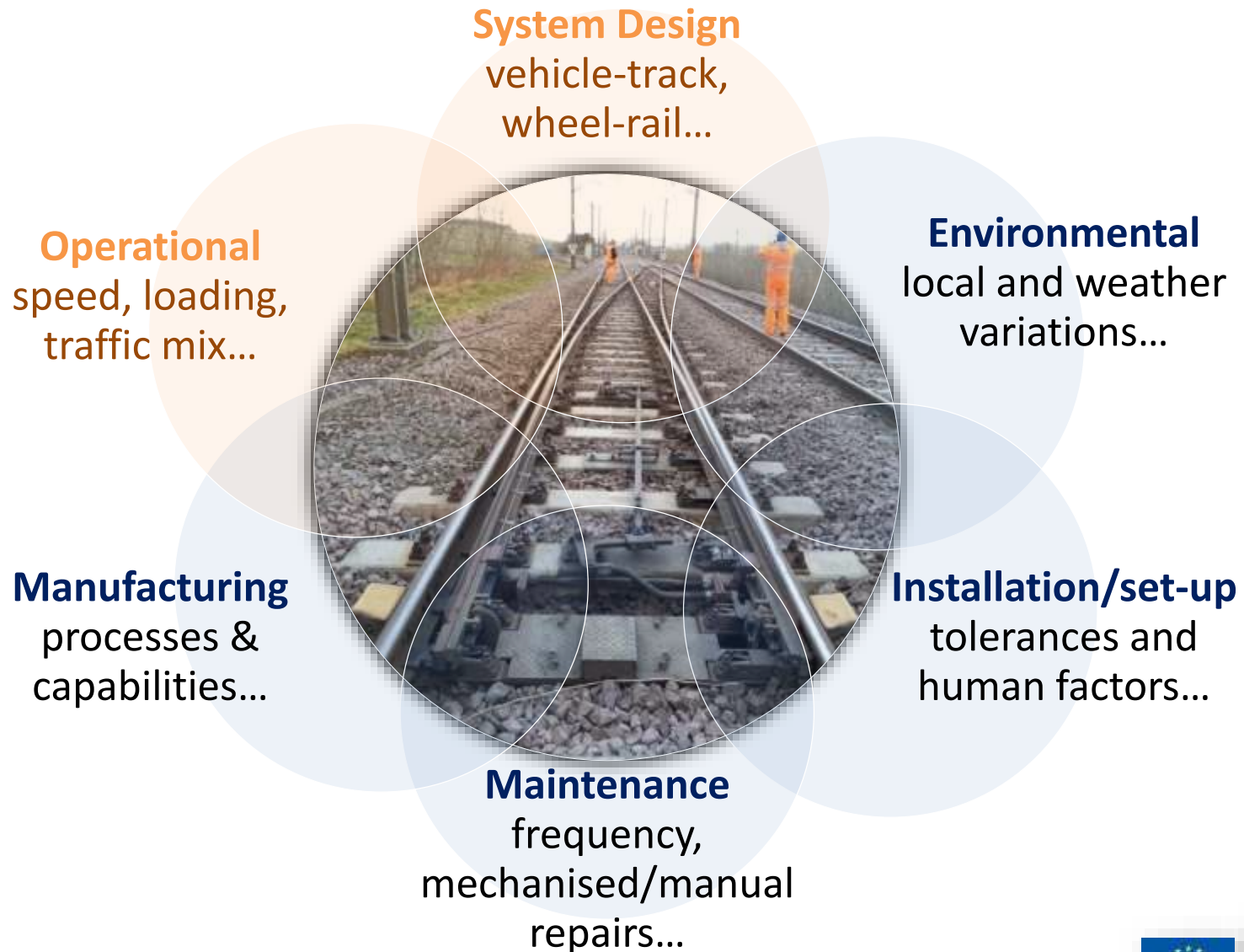
Bearers



# Components damages in S&C



# Root causes

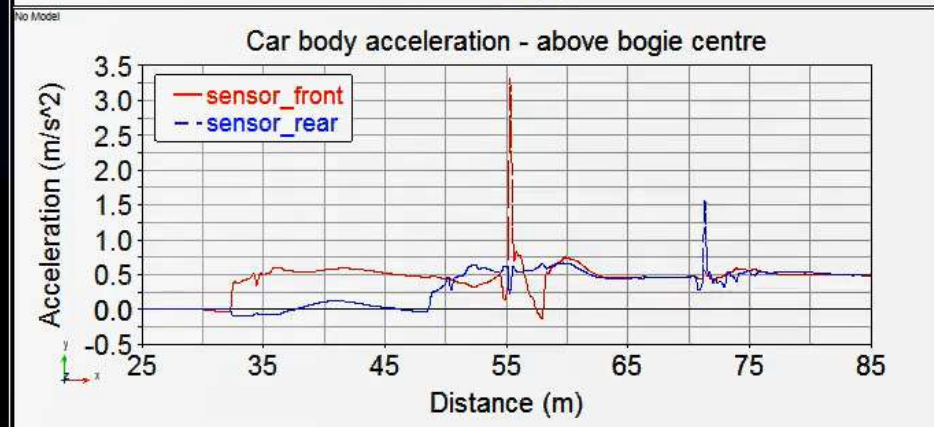
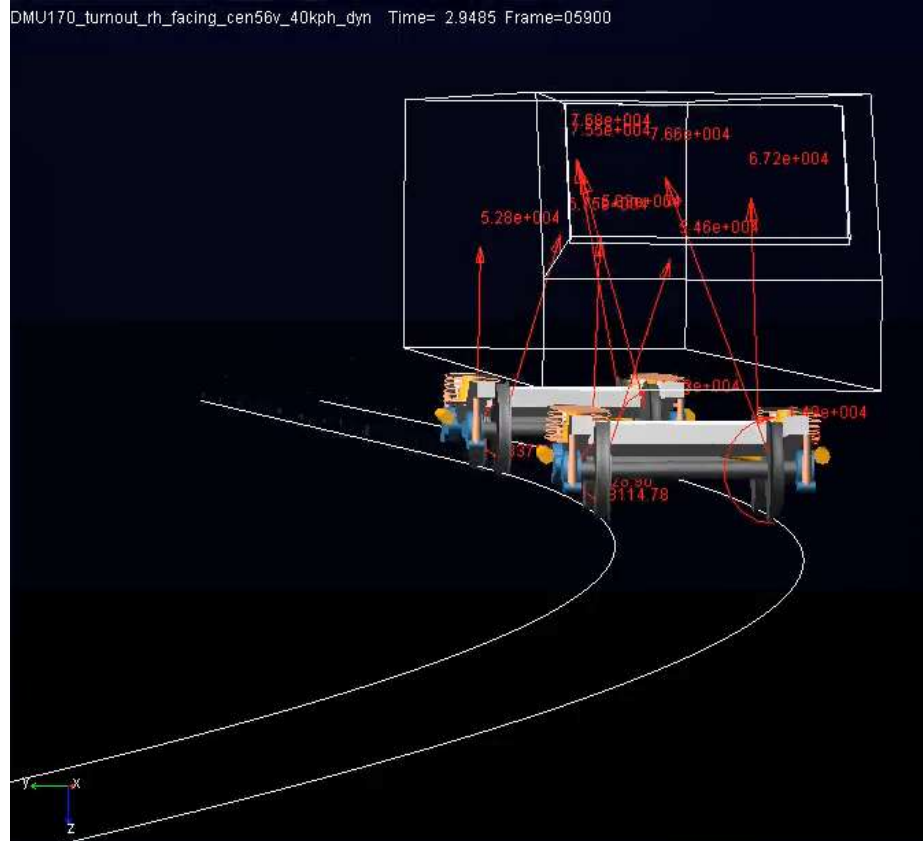




## 2) Vehicle-track and wheel-rail interaction

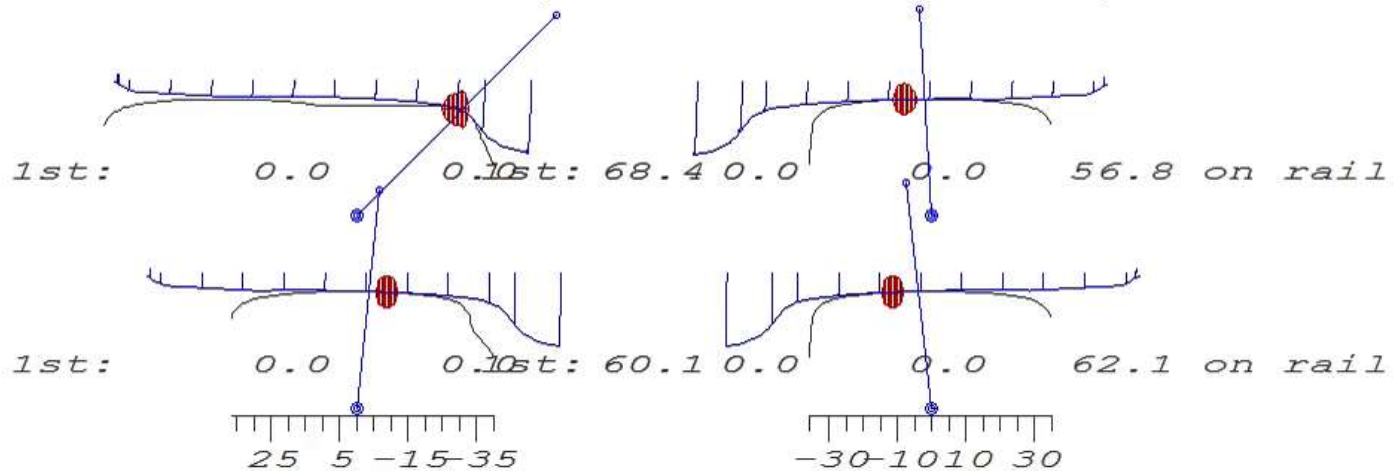






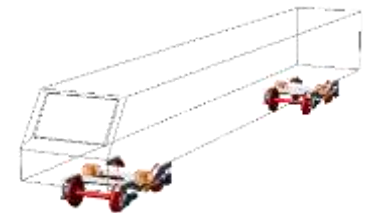
# Fundamental behaviour in S&C

Distance= 32.792m, time= 1.26s, v= 40km/h



Change in rolling radius difference (left/right) as stock rail moves outward and point of contact also

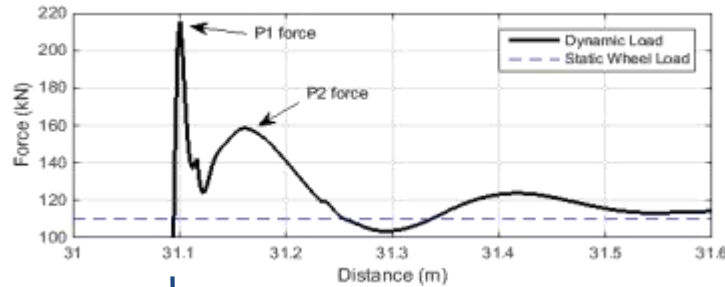
- ↳ induces a steering of the wheelset (angle of attack)
- ↳ and associated lateral steering forces (also the case on through route to a lesser extent)
- ↳ Jump (double) point contact introduces higher frequency force disturbances



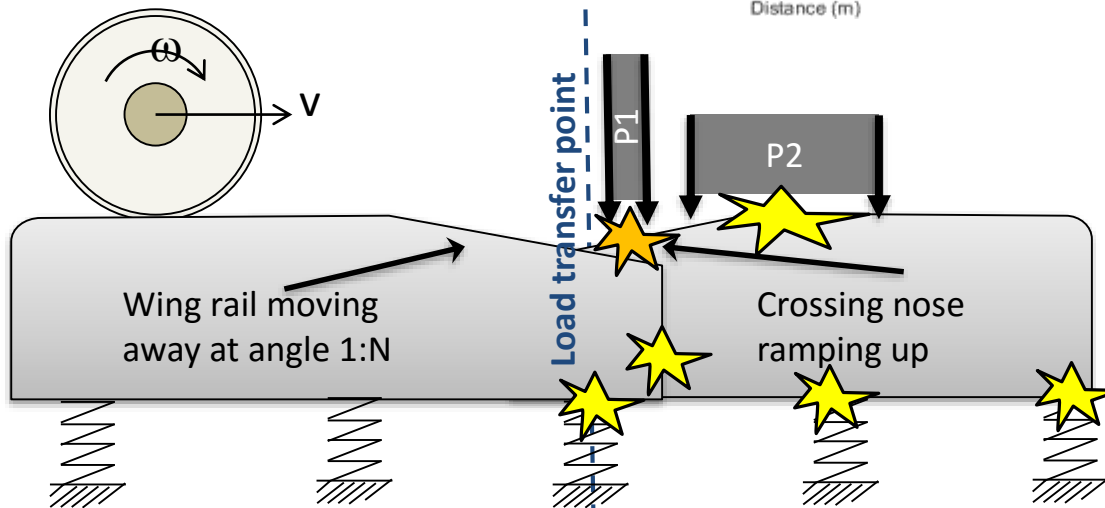
# Fundamental behaviour at crossing

**Key driver:**

- Speed ( $V$ )
- Dip angle ( $\alpha$ )
- Track & wheel mass ( $M$ )
- Track Stiffness ( $K$ )



**Jenkins 74** “The effect of track & vehicle parameters on W-R vertical dynamic forces”



P1 peak position =  $f(V)$  ● → few [cm]

P2 peak position =  $f(V)$  ● → [0.1~0.9m]

**P1**

< 1ms

$f_{cy} \approx 500\text{-}2\text{kHz}$

Wheel and track mass  
Contact stiffness

Rail head damage (plastic deformation, subsurface fatigue) and rail fatigue

**P2**

< 10~20ms

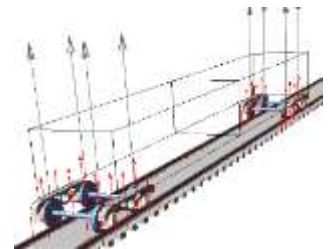
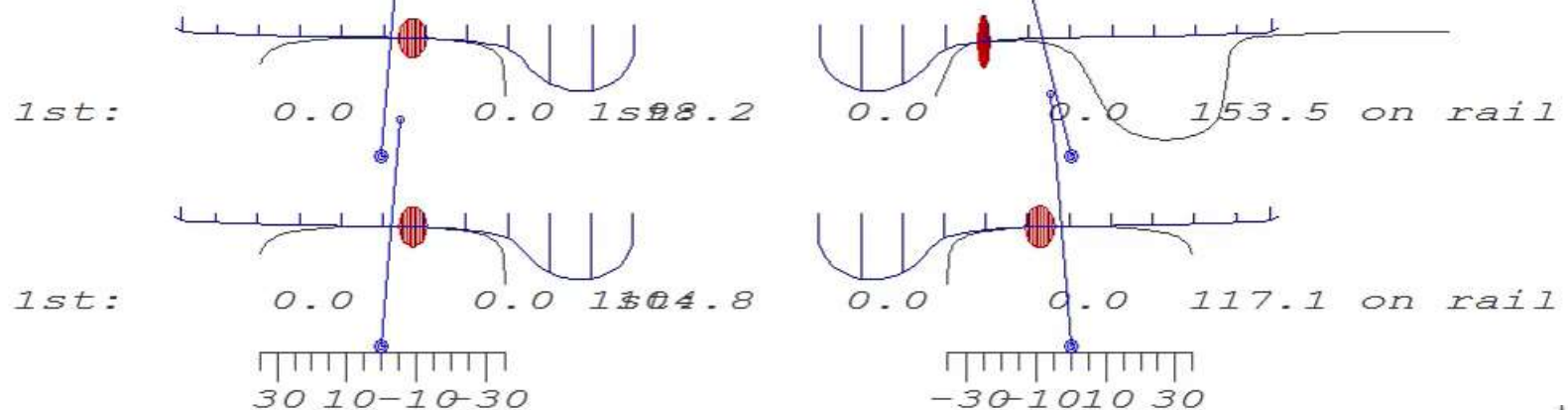
$f_{cy} \approx 50\text{-}120\text{Hz}$

Wheel and track mass, rail elasticity  
Ballast support stiffness

Rail head damage, ballast degradation, sleeper fatigue and rail fatigue

# Fundamental behaviour at crossing

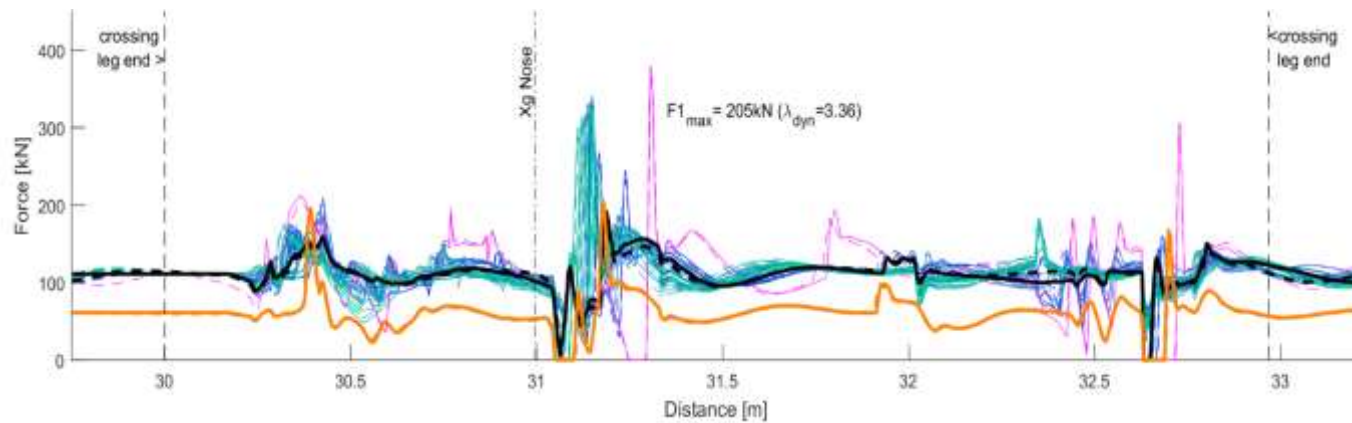
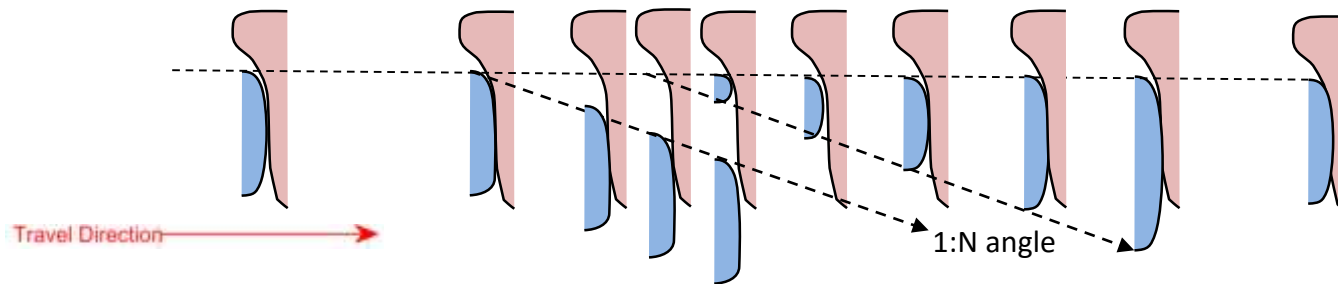
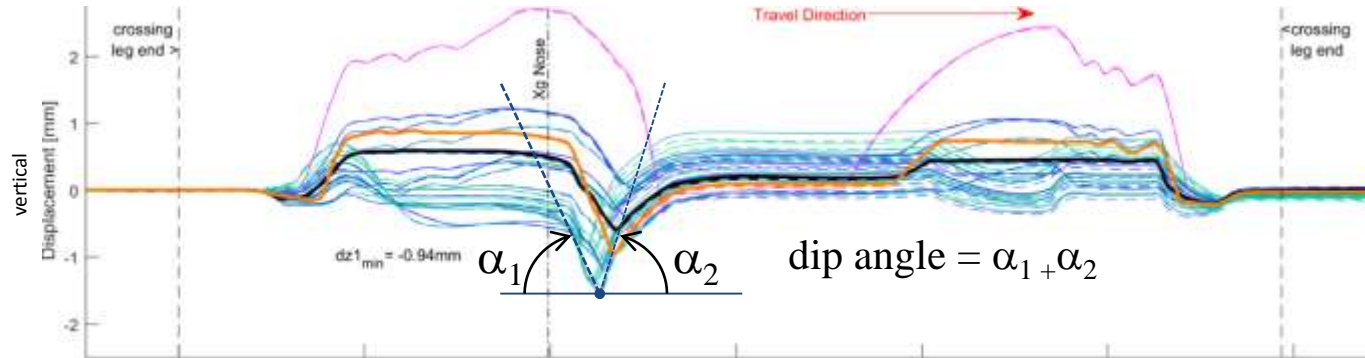
Distance= 31.272m, time= 0.64s, v= 80km/h



- Through the crossing the loading is mainly vertical
- ↳ Although lateral impact load is also present: RRD  $\Rightarrow$  angle of attack + lateral offset in diverging routes
  - ↳ Jump (double) in point contact at entry/exit of casting geometry (smoothed in reality by manual and operational grinding)
  - ↳ Vertical impact at load transfer between wing and nose (vice versa)

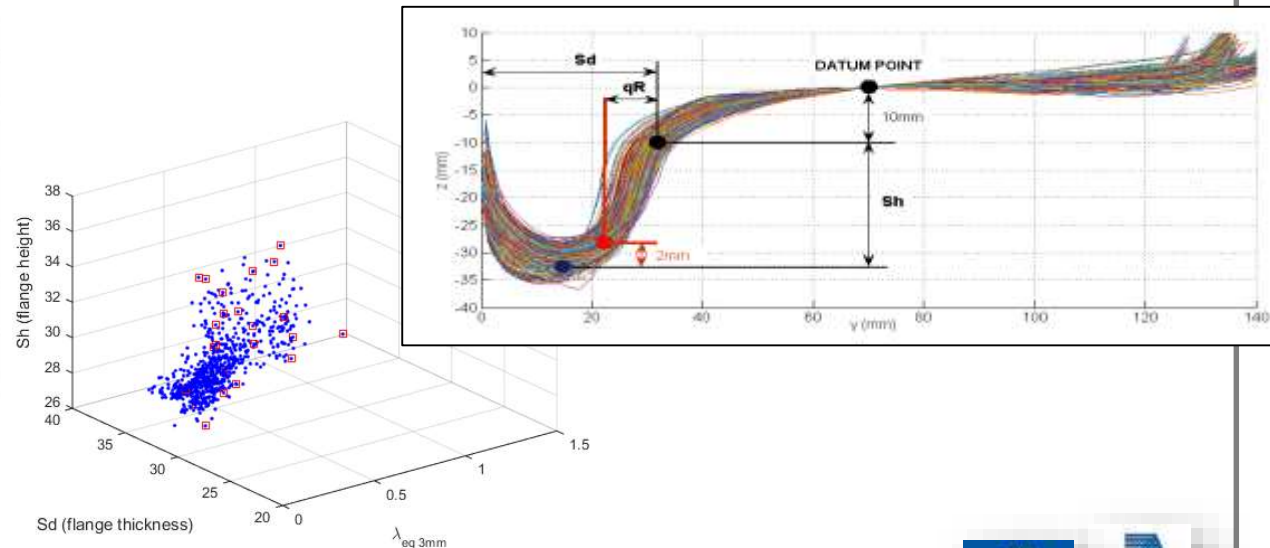
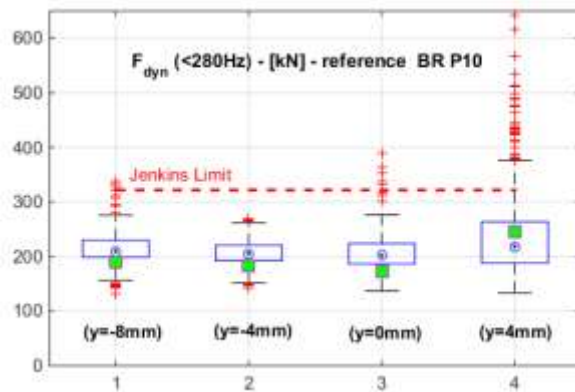


# Fundamental behaviour at crossing



# Fundamental behaviour at crossing

- More parameters affecting reaction forces
  - Range of wheels and crossing geometry shapes
  - Vehicle types and steering ability (PYS)
  - Axles lateral position and angle of attack
  - Track geometry and misalignment
  - Support type and conditions
  - Direction of travel (through/diverging-facing/trailing)

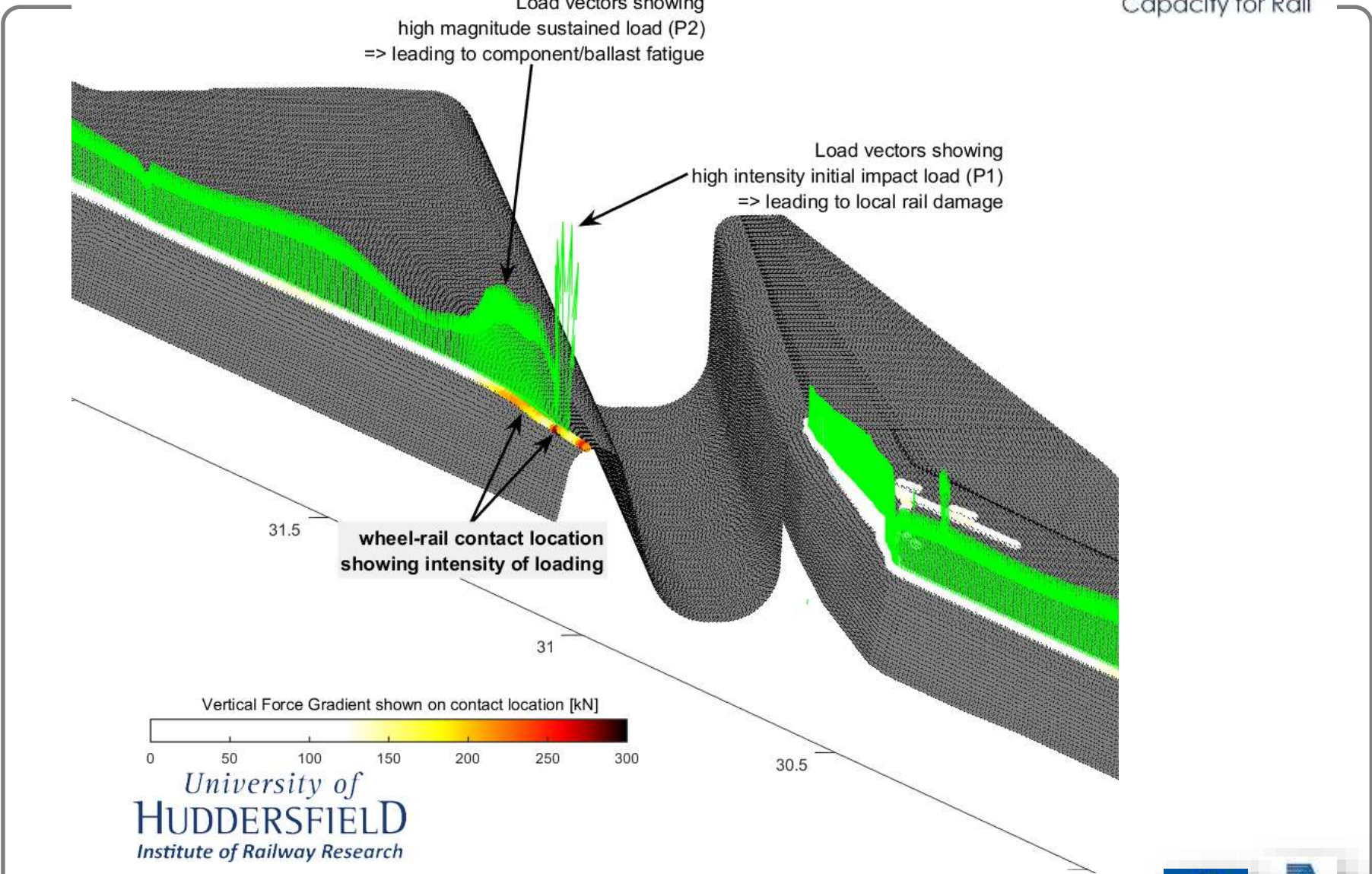


### 3) Predicting damage mechanisms and identifying key drivers



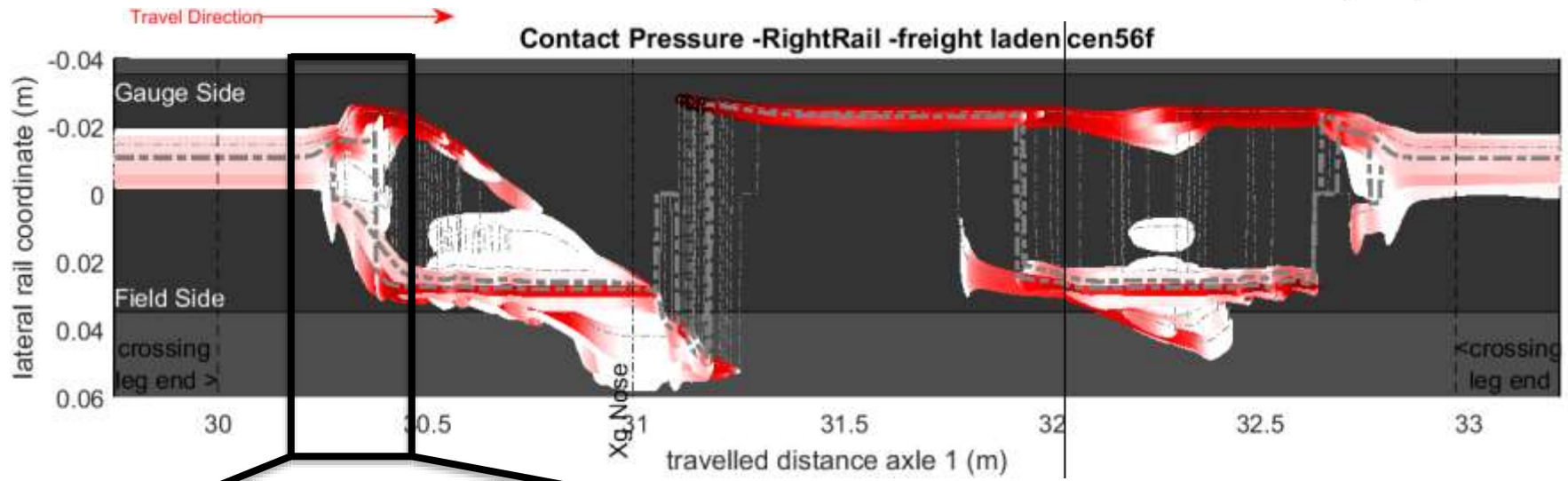


# Observing & predicting damage forces

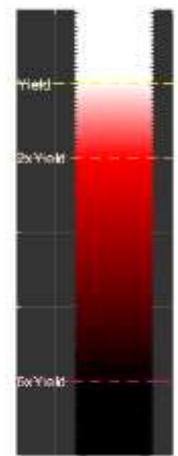




# Observing & predicting w-r interaction

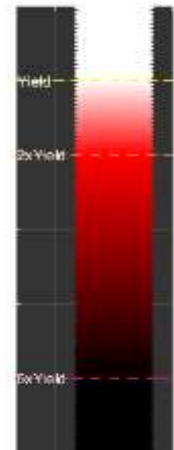
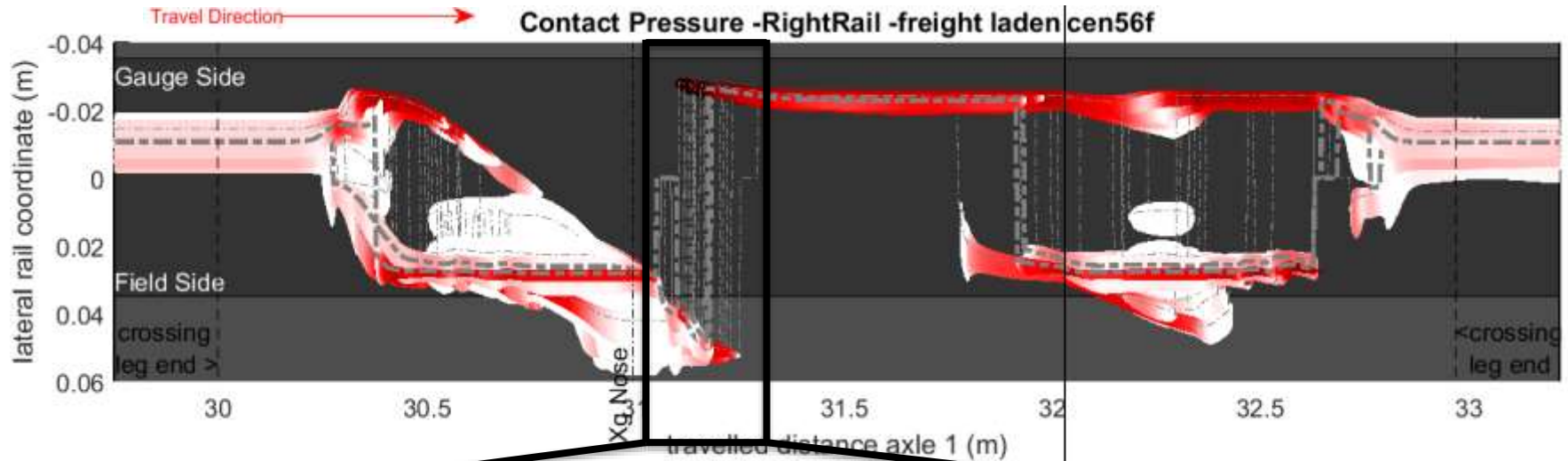


x-dimension not to scale

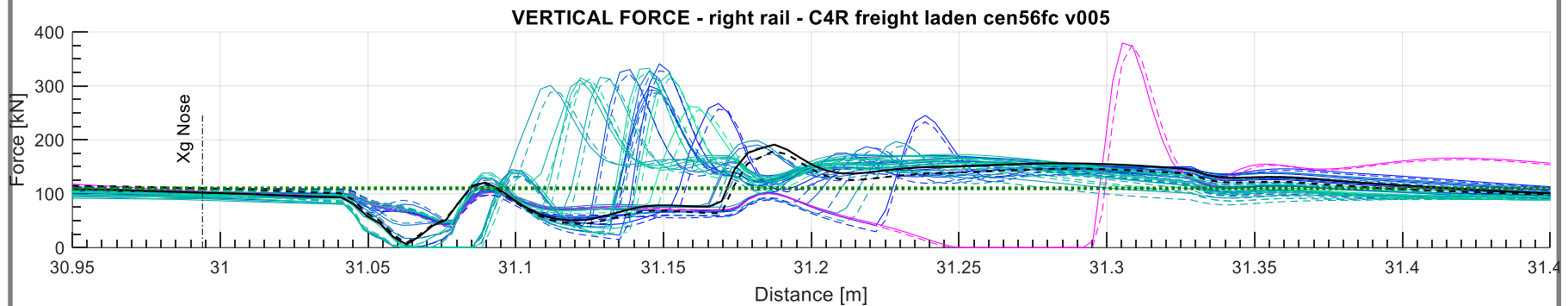


Rapid change of contact in leg ends; multi point contact; high pressure

# Observing & predicting w-r interaction



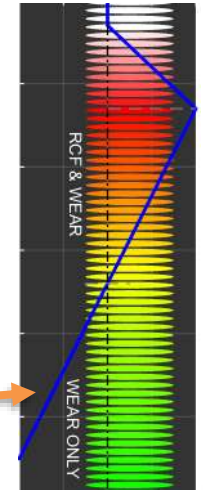
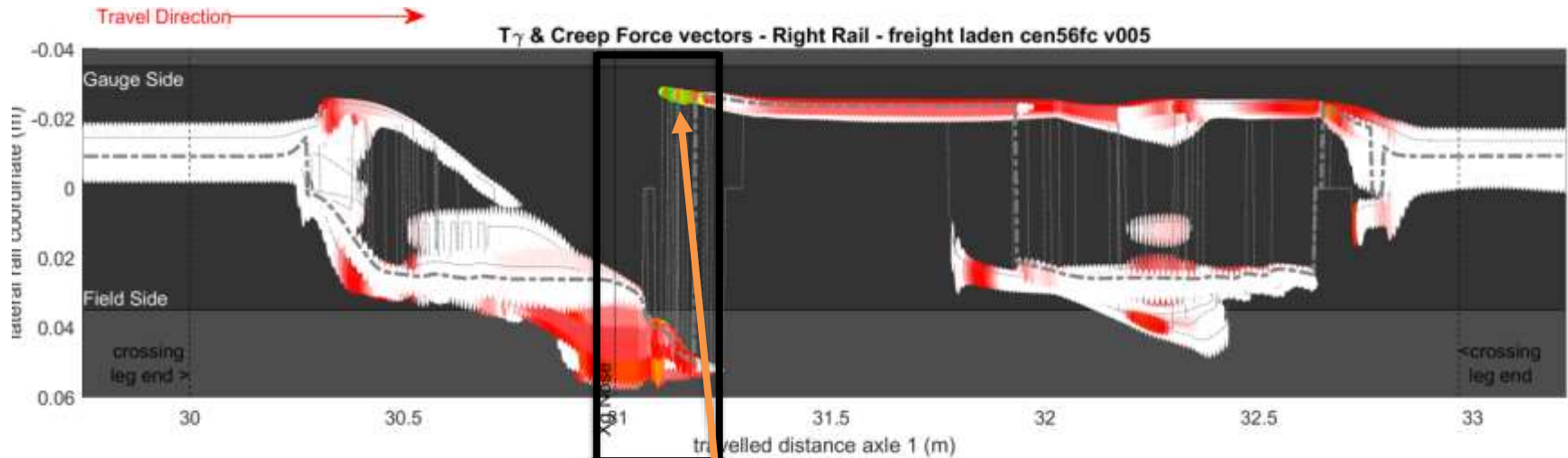
# Observing & predicting w-r interaction



Squats marks corresponding to peak P1 pressure and overall high pressure deformed profiles over P2 action zone



# Observing & predicting w-r interaction



High pressure combined with high wear index on nose



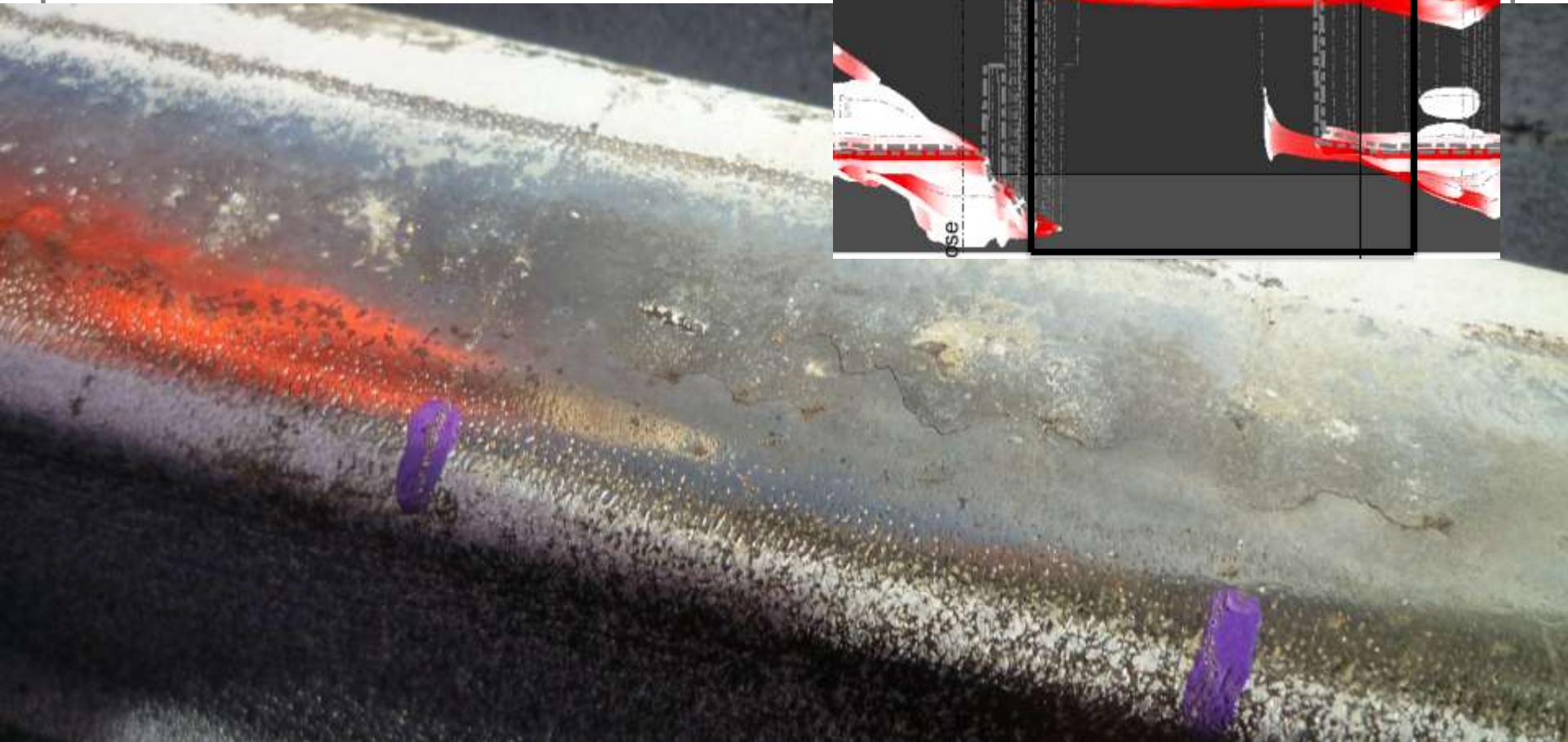
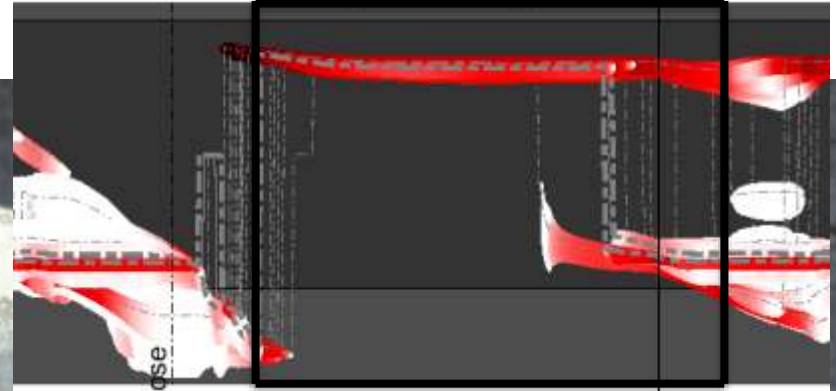
# *Observing & predicting w-r interaction*



High pressure combined with high wear index on nose

# Observing & predicting w-r interaction

Contact Pressure -RightRail -freight laden|cen56f



RCF initiation on crossing vee



## 4) Assessing the benefits of innovations

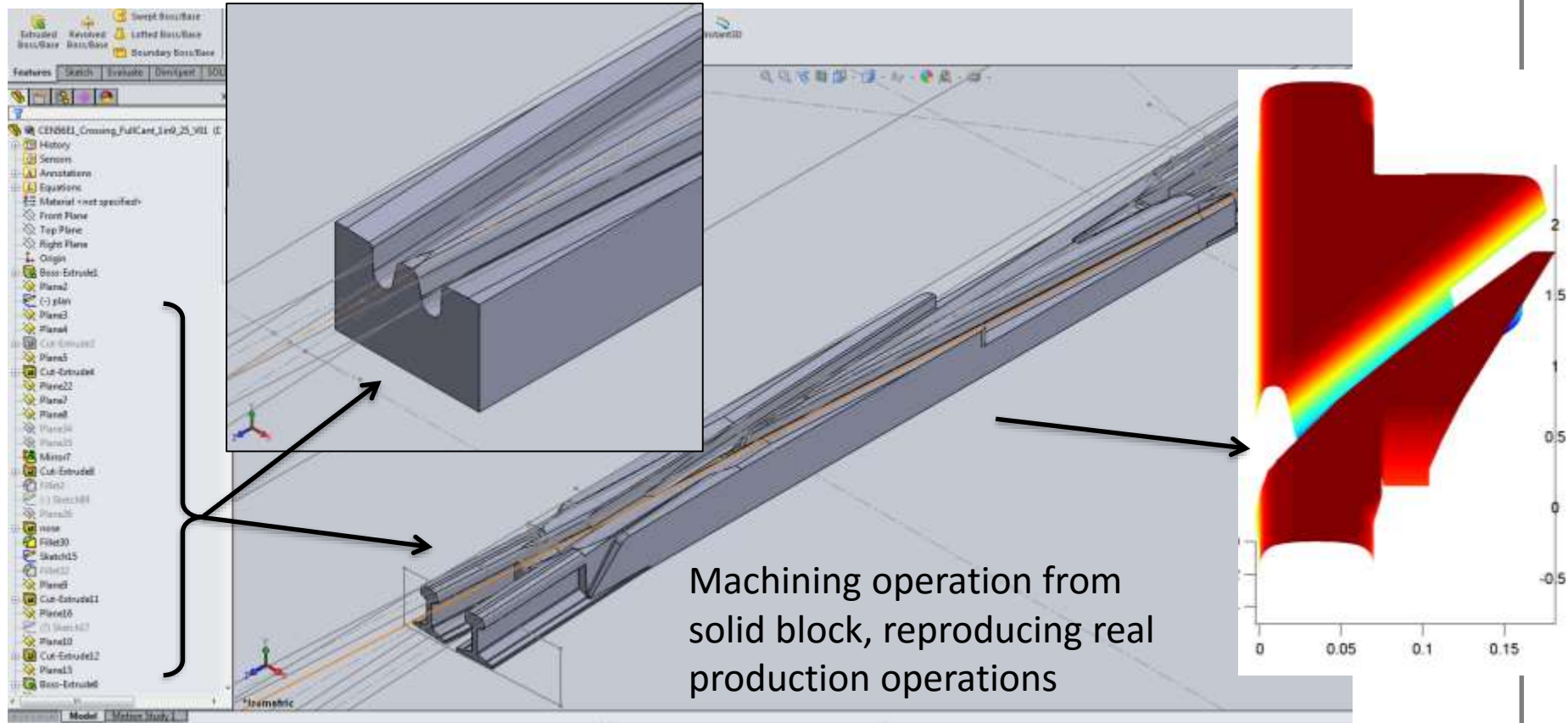


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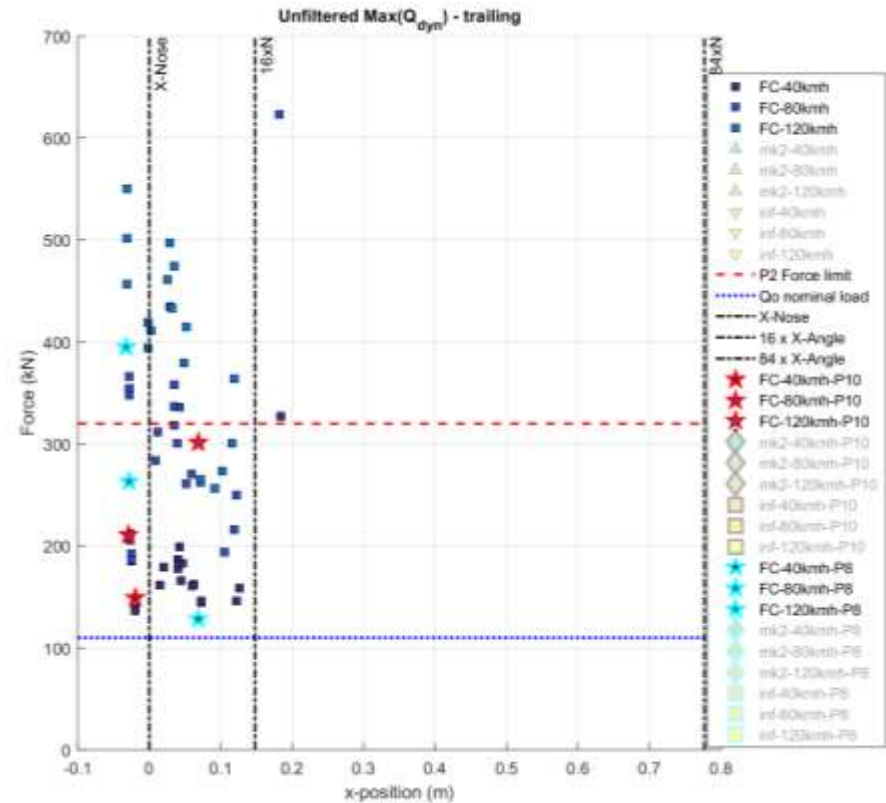
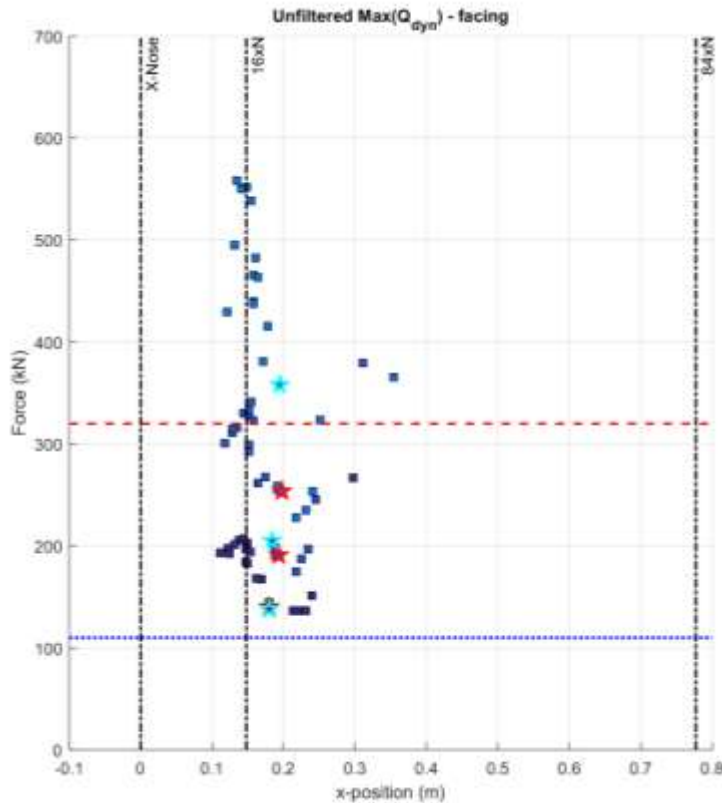


# Assessment of new crossing geometry



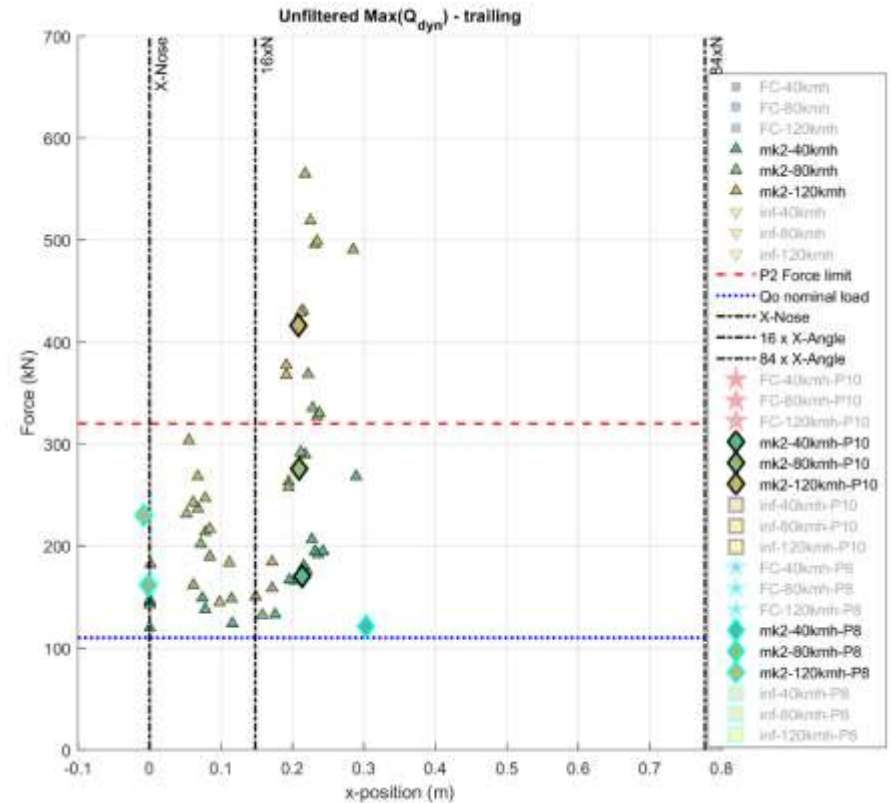
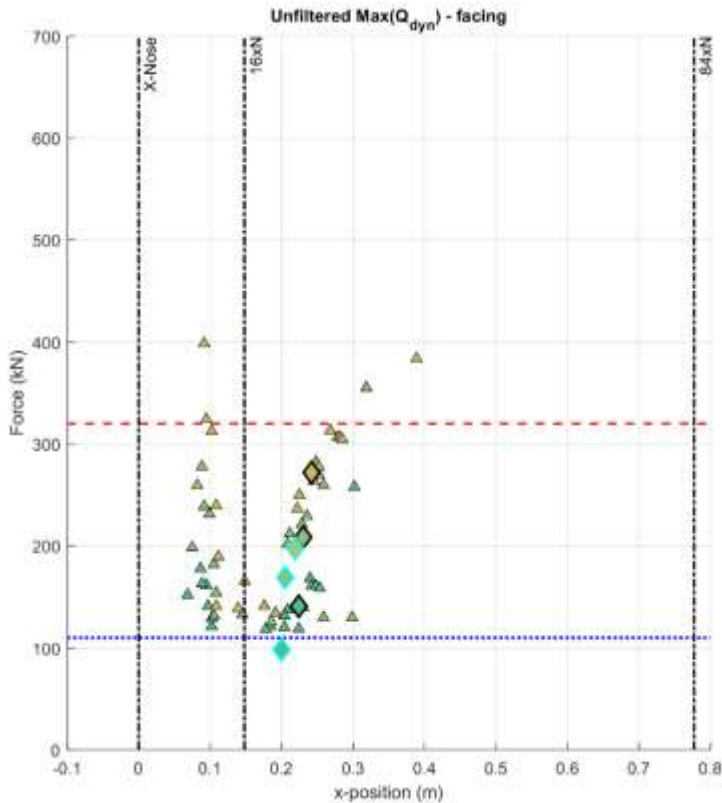
Comparative study of 4 different UK crossing designs in use:  
CEN56 vertical and inclined, NR60 existing and improved

# Assessment of new crossing geometry



P1 vs load transfer position - CEN56c

# Assessment of new crossing geometry

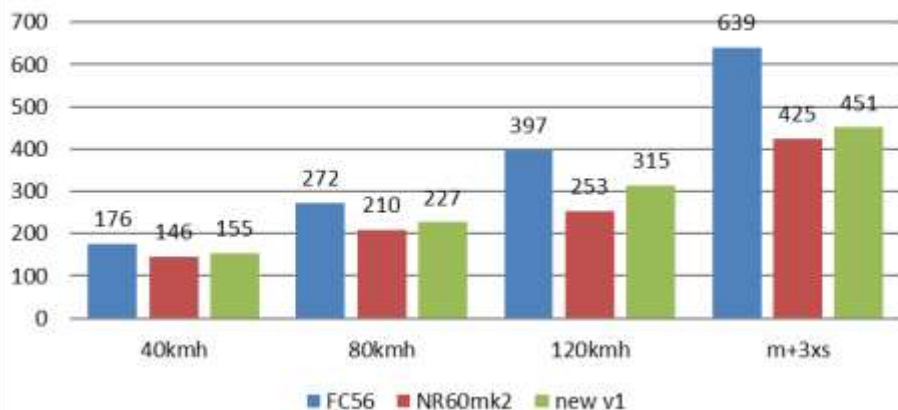


P1 vs load transfer position - NR60

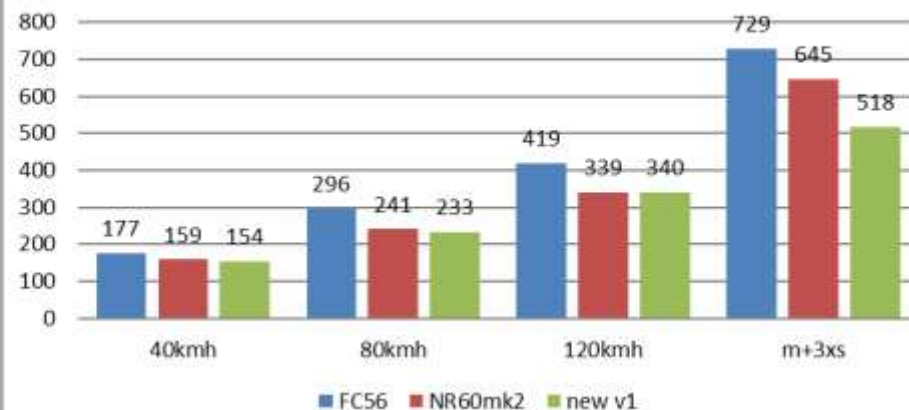


# Assessment of new crossing geometry

## FACING average P1 forces



## TRAILING average P1 forces



	FACING average P1 forces			TRAILING average P1 forces		
	FC56	NR60mk2	new v1	FC56	NR60mk2	new v1
40kmh	0%	-17%	-12%	0%	-10%	-13%
80kmh	0%	-23%	-17%	0%	-19%	-21%
120kmh	0%	-36%	-21%	0%	-19%	-19%
average	0%	-28%	-18%	0%	-17%	-19%
SD	0%	-38%	-39%	0%	-8%	-36%
$\mu+3\sigma$	0%	-33%	-29%	0%	-12%	-29%

- Geometry
  - Smooth changes (avoid contact jumps) and more conformal shapes
  - Ensure compliance with a wide range of representative wheels shapes
  - Minimise dip angle (geometrical calculation)
- Support
  - Use of USP, shorter sleeper spacing, resilient baseplate systems
  - Hybrid tracks > slab track
- Materials
  - Better resisting material for nose, wing, switches
- Monitoring
  - Profile geometry measurement (at regular time intervals)
  - Geometry monitoring (alignment in switch panel)
  - Vibration analysis (finding and eliminating high damage instances)
    - Track-side
    - On-board vehicles
      - Instrumented wheelset (not high frequencies enough)
      - Axle box accelerations (need to be tuned for HF + data collection) and need to know positions of S&C

- S&C attract disproportionate amount of damage and costs
- Careful wheel-rail geometry interaction can significantly improve system performance from design through to continuous monitoring for sustained performance
- Support discontinuity should be ‘bridged’ using more resilient layers (baseplate on resilient pad) and better load distribution within the superstructure and support layers
- High impact load instances can be monitored and ruled out, this requires both track side and vehicle based instrumentations and intelligence
- Numerical simulation together with site observation/measurement can offer a unique view of the system interaction
- Finally, simple rules and algorithm can be derived from studies as presented here for a more direct industrial applications



*Thank you for your kind attention*

**Bezin Yann**

*Head of Research*

*Institute of Railway Research*

University of Huddersfield

[y.bezin@hud.ac.uk](mailto:y.bezin@hud.ac.uk)

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